Miniature curved artificial compound eyes

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In most animal species, vision is mediated by compound eyes, which offer lower resolution than vertebrate single-lens eyes, but significantly larger fields of view with negligible distortion and spherical aberration, as well as high temporal resolution in a tiny package. Compound eyes are ideally suited for fast panoramic motion perception. Engineering a miniature artificial compound eye is challenging because it requires accurate alignment of photoreceptive and optical components on a curved surface. Here, we describe a unique design method for biomimetic compound eyes featuring a panoramic, undistorted field of view in a very thin package. The design consists of three planar layers of separately produced arrays, namely, a microlens array, a neuromorphic photodetector array, and a flexible printed circuit board that are stacked, cut, and curved to produce a mechanically flexible imager. Following this method, we have prototyped and characterized an artificial compound eye bearing a hemispherical field of view with embedded and programmable low-power signal processing, high temporal resolution, and local adaptation to illumination. The prototyped artificial compound eye possesses several characteristics similar to the eye of the fruit fly Drosophila and other arthropod species. This design method opens up additional vistas for a broad range of applications in which wide field motion detection is at a premium, such as collision-free navigation of terrestrial and aerospace vehicles, and for the experimental testing of insect vision theories.

Fabrication Process

Design Method. As with biological compound eyes, CurvACE artificial ommatidia consist of three materially and functionally different layers (Fig. 2A): (i) an optical layer composed of an array of highly transparent polymer microlenses molded on a glass carrier (Fig. S1), which focus light precisely onto (ii) the sensitive areas of a silicon-based photodetector layer. This layer contains an array of analog very-large-scale integration (VLSI) photodetectors as well as additional circuitry to condition the signal for processing (Fig. S2). Finally, (iii) a flexible electromechanical interconnection layer, formed by a polyimide printed circuit board (PCB), physically supports the ensemble and transfers the output signals from the individual ommatidia (Fig. 2B) to the processing units. With thicknesses of 550 μm, 300 μm, and 100 μm, respectively, the total...
Fabrication of a CurvACE Prototype. We fabricated a CurvACE prototype by bending a rectangular array of 42 columns of 15 artificial ommatidia (micro lenses diameter = 172 μm) down to a curvature radius of 6.4 μm along its longer direction, to yield a total FOV in the horizontal plane (Fig. 1 A and B and Fig. S3 B and C). This curvature should nominally yield an interommatidial angle Δφ of 4.3° in the equatorial row along the bent direction. Although there is no mechanical bending along the vertical direction, it is possible to make the visual axes of the 15 ommatidia in each column fan out in the vertical plane by making the vertical pitch between the photodetectors stepwise smaller than the vertical pitch between the micro lenses (10) (Fig. SIC). In the prototype, the photodetector pitch was calculated so as to obtain a similar value for the interommatidial angle Δφ along the vertical unbent direction, which results in a total vertical FOV of 60° (Fig. IB). To avoid spatial aliasing or blind spots in the visual field, the acceptance angle Δφ of each ommatidium must closely approach the interommatidial angle Δφ (1, 24) (Fig. 3C). Therefore, the ommatidial lenses, diaphragms, and photodetectors were designed using an optical ray tracing technique (Zemax; Radiant Zemax, LLC) to produce an acceptance angle Δφ of 4.3°.

The resulting concavity on the backside of the prototype after the mechanical bending along the horizontal direction is used to host two microcontrollers, two inertial sensors, and other electronic components that are fitted and soldered on two rigid PCBs (Fig. 2D and Figs. S3C and S4). In the experiments described below, the embedded microcontrollers are programmed to operate the visual data read-out and communicate with an external computer for analysis; in a stand-alone application, these microcontrollers can be used to process visual data onboard the prototype without any external computer.

Results
Characterization of Visual Sampling. To characterize the visual sampling of the environment by the fabricated CurvACE prototype, we measured the angular sensitivity function (ASF) of each of the 630 artificial ommatidia (Fig. S5). Fig. 3 A and D shows representative examples of ASFs measured along a single row and a single column, respectively. Most ASFs display the expected Gaussian distribution with respect to the light incidence angle, which validates both the microoptical design and the precise alignment with each individual photodetector. We derived the experimental acceptance angles and interommatidial angles from the measured ASFs. The acceptance angle Δφ of an ommatidium is defined as the full width at half maximum (FWHM) of its Gaussian-like ASF. The horizontal and vertical interommatidial angles ΔφH and ΔφV were assessed from the angular position of the peak of the ASFs of two adjacent ommatidia (Fig. 3C). The measured acceptance angles yielded an average of Δφ of 4.2° ± 0.3° (SD) for both
horizontal (Fig. 3A) and vertical (Fig. 3D) directions. The vertical interommatidial angles resulted in an average of $\Delta \phi_v = 4.26^\circ \pm 0.16^\circ$ (SD) (Fig. 3D), and the horizontal ones ranged from $\Delta \phi_h = 4.2^\circ \pm 0.8^\circ$ (SD) in the middle row (Fig. 3A) to $3.7^\circ \pm 0.7^\circ$ (SD) in the top and bottom rows (Fig. 3B). The close match between the experimentally measured acceptance angles and interommatidial angles validates both the ray-tracing design and fabrication process while indicating that the CurvACE prototype, like the...
fruit fly compound eye (24), performs an adequate sampling of its entire FOV (Fig. 1B). The observed spread in the values of the horizontal interommatidial angles $\Delta\phi_h$ (Fig. 3 A and B) is probably due to the manual process used to mechanically fix the flexible PCB supporting the artificial ommatidia array onto the rigid curved substrate.

Characterization of Ommatidium Light Adaptation. In the natural world, visual sensors must cope with a wide dynamic range of irradiance, which can span on the order of 8 decades over the course of a day. Light variations within a scene are particularly challenging because they can make part of the visual field nonresponsive due to photoreceptor saturation. Animal retinas partly solve this crucial problem by means of a local light adaptation mechanism integrated within each photoreceptor (3, 4, 25, 26). Similarly, we have equipped each prototype ommatidium with a neuromorphic adaptation circuit (Fig. S2D) that operates independent of its 629 neighbors. The neuromorphic circuit originally proposed by Delbrück and Mead (27) was modified here by cascadimg a first-order, low-pass filter (Fig. S2D). This modification prevents temporal aliasing and keeps the photodetector bandwidth of 300 Hz practically constant across the entire studied range of ambient lighting conditions. The circuit design was further optimized (SI Text, Photodetector Layer) to minimize the transient gain dispersion of each autoadaptive circuit. Fig. 4 shows the mean steady state and transient responses of 11 artificial ommatidia (photodetectors with optics) in one column to light step increments and decrements presented at four different steady light levels (Fig. S6). At each of these four levels (red circles in Fig. 4), the output response of the individual ommatidia to light steps yields an S-shaped operating curve in a semilog plot. Adaptation to a novel steady irradiance level essentially produces a horizontal shift of the curve without markedly changing its slope, which represents a dynamic sensitivity of about 1,300 mV per decade in the linear part. The steady operating curve (shown in red in Fig. 4) is also a logarithmic function of the adapting light, but with a slope (steady sensitivity) about 12-fold smaller. Thanks to the optimized design of the adaptive photodetector layout, the averaged dispersion of the sensitivity over the four operating curves is as small as 11 mV, that is, only about 2% of the total 600-mV dynamic range.

The four operating curves demonstrate not only the high sensitivity of the prototype ommatidia but their relative invariance in sensitivity to the ambient light. These $V(\log I)$ curves shifting with the operating points are reminiscent of those obtained in analogous experiments carried out on single vertebrate (25) and invertebrate (26) photoreceptors. This local adaptation is essential for efficient sampling of natural environments because it prevents saturation of the photoreceptors by bright spots in the visual scene while allowing them to adapt quickly to untoward illumination changes, such as transitions from a shaded area to a sunny place.

Characterization of Motion Extraction. In addition to an extensive FOV (Fig. 3) and local adaptation to illumination (Fig. 4), the CurvACE prototype ommatidia yield a signal acquisition bandwidth of 300 Hz, which is threefold higher than that measured in the ommatidia of fast-flying insects (28). A high bandwidth contributes to the reduction of motion aliasing during fast locomotion. Furthermore, the implemented read-out protocol (Fig. S7) allows a maximum frame rate of 1.5 kfps, which permits frame averaging to improve the signal-to-noise ratio. We experimentally tested CurvACE motion detection capabilities by computing optic flow vectors from visual signals resulting from different types of motion in the presence of random black and white patterns on a wall (Fig. S8). In this first experiment, we used a modified version of the Lucas–Kanade method (29, 30) (SI Text, Optic Flow Characterization and Eqs. S1–S9), which is a particularly efficient image-based processing algorithm used to calculate optic flow vectors in two dimensions. The optic flow vectors measured during roll rotation (Fig. S4) and linear translation toward a textured wall 0.3 s before collision (Fig. S5B) show coherent patterns of visual rotation and expansion, respectively. The center of rotation and focus of expansion can be clearly identified (red dots in Fig. 5), allowing for estimation of the axis of rotation and of the direction of translation, respectively. The sensor egomotion can be estimated from these flow fields, for instance, by implementing matched filters (31) analogous to the directionally selective, motion-sensitive neurons found in some insect visual systems (5). Furthermore, the embedded inertial sensors can be used for cancelling the rotational component of the measured optic flow, assessing only the translational component. Because this component is related to distance from objects, the optic flow data provided by a CurvACE prototype could assist mobile platforms to perform collision-free navigation (9).

We also characterized motion detection quantitatively at different ambient light levels with a bioinspired local visual processing
algorithm based on the “time-of-travel” scheme (32) (Fig. S9). Fig. 6 shows the angular speed $\Omega_{\text{yaw}}$ obtained by measuring the rotational optic flow as a function of the yaw rotational speed of CurvACE surrounded by a natural pattern. The experimental data show a good match between the rotational speed perceived by CurvACE and the true rotational speed. The error in the regression coefficient (linearity error) ranges from 5 to 10% (Fig. 6) at the three illumination levels, indicating that the CurvACE sensor takes full advantage of its autoadaptive analog VLSI photodetectors to make motion detection largely invariant to different illumination conditions. With the time-of-travel scheme, any pair of neighboring ommatidia driving a “local motion sensor” is able to measure angular velocities ranging from 50° to 358° per second for the interommatidial angle of 4.2° with sufficient accuracy. Measurement limitation at lower speeds is due to the signal attenuation brought about by the spatiotemporal processing present in each artificial ommatidium (Fig. S9A).

Discussion

The prototype presented here represents one of many possible manifestations of the CurvACE design principle. It yields a compact, lightweight, energy-efficient, miniature vision sensor that suits a broad range of applications requiring fast motion detection across a panoramic FOV. The applied optical and electronic parameters enable this prototype to measure optic flow patterns caused by sensor egomotion within a contrasted environment. A prototype with these characteristics could be used for autonomous terrestrial navigation, in analogy with some crab species (33) that use quasicylindrical compound eyes to navigate in flat environments. Furthermore, the hemispherical FOV of the prototype obtained by horizontal bending and by the longer microlens vertical pitch distance resembles the FOV of flying insects (1). Thus, such a prototype could also be used in Micro Air Vehicles (MAV) to support a large number of navigation tasks, such as egomotion estimation (34), collision avoidance (6, 7), and flight control (8, 9, 35), at low and high speeds, even in complex indoor and outdoor environments.

The CurvACE design principle also allows for flexible customization of artificial ommatidia in terms of their number, size, focal length, and interommatidial and acceptance angles, according to the requirements of the intended use. The artificial ommatidia could be further tailored by taking inspiration from the extraordinary eye regionalization found in insects and crustaceans, where specific parts of the compound eye serve specific functions. For example, higher acuity (36) may be obtained by increasing ommatidial resolution in defined areas, which could be achieved by decreasing both the acceptance angle and the interommatidial angle through redesigned microlenses and a reduced photodetector size with a consequent loss of signal-to-noise ratio. Design variations in the ommatidial optics or photodetector characteristics could yield regions of higher light capture (37) or different spectral (38) or polarization sensitivity (39).

The size of the CurvACE prototype described here is comparable to that of some trilobite eyes (22) (Fig. 1C) and some crab eyes (33), but reaching the diminutive size of insect eyes is challenging because it implies various tradeoffs. Increasing the surface density of artificial ommatidia requires decreasing photosensor size, chip circuitry, and microlens diameter at the cost of lower sensitivity and signal-to-noise ratio. Considering state-of-the-art technologies, we have estimated that the CurvACE prototype could be further reduced by a factor of 2. Further increments of surface density via hexagonal arrangement of ommatidia, similar to that found in many insect eyes, may be possible but would require different cutting methods. In the future, the development of vertical integration of 3D electronic circuits could further reduce the footprint size at the cost of chip thickness.

The CurvACE design opens up new avenues for vision sensors with alternative morphologies and FOVs of up to 360° in small, compact packages. In particular, the realization of a fully cylindrical CurvACE with a 360° FOV in the horizontal plane is relatively straightforward, either by attaching two semicylindrical prototypes (Fig. S4D) or by fabricating a wider array with a larger number of ommatidia. A CurvACE prototype with a truly omnidirectional FOV, reminiscent of the eye morphology of most...
flying insects, would be especially interesting for egomotion estimation and better navigational support in three dimensions in a minimal package, providing an advantageous alternative to current cumbersome arrangements based on catadioptric or fish-eye lenses (9). A spherical CurvACE could be realized by fabricating and individually bending several ommatidial arrays with one ommatidium per column along the meridians of a sphere to measure optic flow omnidirectionally.

The CurvACE design is expected to foster further research and applications on fully flexible vision sensors (40, 41) that can adapt to rigid or unsteady surfaces of arbitrary shapes. Such devices could function as thin wearable sensors on smart clothing, as sensors for intelligent homes, or integrated in the artificial skin of soft robots. Toward these applications, future work could devise methods for cost-effective mass production of artificial ommatidia, which would also allow more complex dicing to achieve alternative bending patterns. Such production methods may include the realization of all processes of ommatidia alignment and assembly at the wafer level with the help of robotic platforms for automated pick-and-place, bonding, and dicing.

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